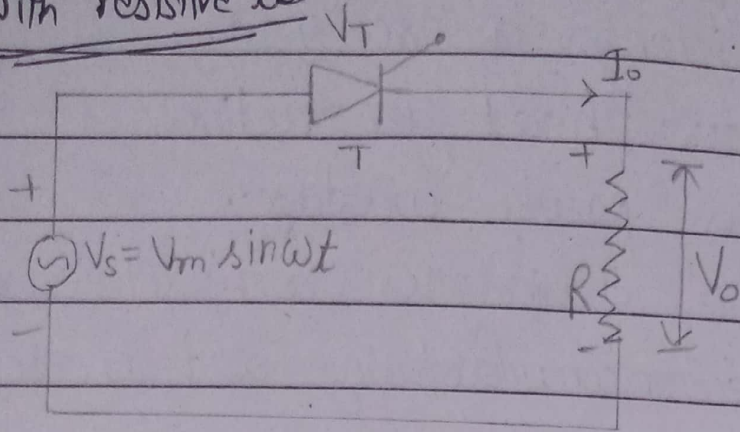


# Single Phase Half-Wave Rectifiers - With resistive load



It consists of a SCR, AC voltage source ( $V_s$ ) & load. The load may be purely resistive, inductive or RL load.

A thyristor blocks the flow of load current ( $I_o$ ) until it is triggered. At some delay angle ( $\alpha$ ), a +ve gate signal applied b/w gate & cathode turns on the SCR.

Immediately full supply voltage is applied to load as  $V_o$ . At the instant of delay angle ( $\alpha$ ),  $V_o$  rises upto  $V_s$  i.e.,  $V_m \sin \omega t$  for resistive load  $I_o$  is in phase with  $V_o$ .

But as soon as the  $V_s$  becomes zero at  $\omega t = \pi, 3\pi$  etc., the load current will become zero & after  $\omega t = \pi$ , SCR is reversed biased & T will turn off at  $\omega t = \pi$ . Thyristor will remain in off condition till it is fired again at  $\omega t = (2\pi + \alpha)$  after delay ( $\alpha$ ).

Thyristor remains ON from  $\omega t = \alpha + \pi$ ,  $(2\pi + \alpha)$  to  $3\pi$  etc., during these intervals  $V_T \neq 0$ . It is OFF from  $\pi$  to  $(2\pi + \alpha)$ ,  $3\pi$  to  $(4\pi + \alpha)$  etc. during these intervals  $V_T$  has the waveshapes of  $V_s$ .

$$V_s = V_o + V_T$$

As we know, avg. value of funct<sup>n</sup>  $f(x)$

$$\text{Avg. value} = \frac{1}{T} \int_0^T f(x) \cdot dt$$

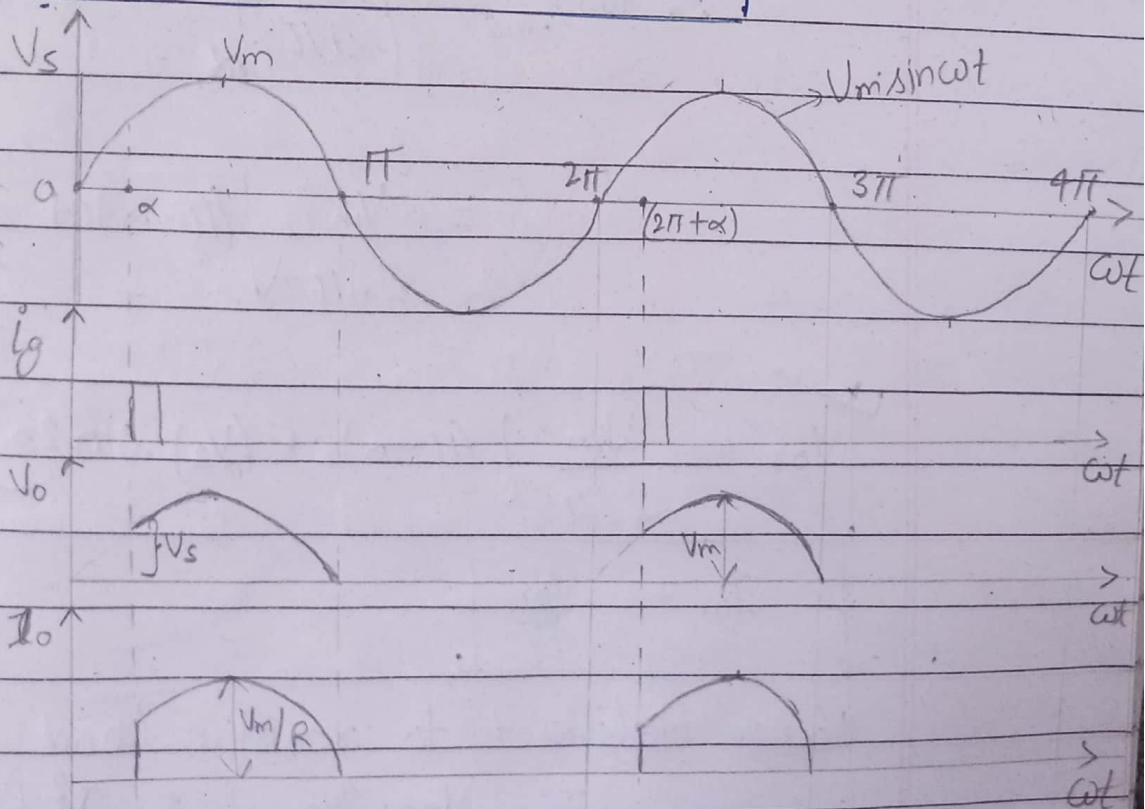
$$\therefore \text{Avg. value of } V_o = \frac{1}{2\pi} \int_0^{2\pi} V_m \cdot \sin \omega t \cdot d(\omega t)$$

$$\therefore V_o = 0 \text{ at } 0 \leq \omega t \leq \alpha \text{ \& } \pi \leq \omega t < 2\pi$$

$$\therefore \text{Avg. } V_o = \frac{1}{2\pi} \int_{\alpha}^{\pi} V_m \cdot \sin \omega t \cdot d(\omega t)$$

$$= \frac{V_m}{2\pi} (1 + \cos \alpha)$$

$$(V_o)_{\text{avg.}} = \frac{V_m}{2\pi} (1 + \cos \alpha)$$



# RMS value of funct<sup>n</sup> $f(x)$

$$f(x)_{\text{rms}} = \sqrt{\frac{1}{T} \int_0^T [f(x)]^2 dx}$$

$$\therefore (V_0)_{\text{rms}} = \sqrt{\frac{1}{2\pi} \int_0^{2\pi} V_m^2 \sin^2 \omega t \cdot d(\omega t)}$$

$$= \left[ \frac{V_m}{4\pi} \int_0^{2\pi} (2 \sin \omega t)^2 \cdot d(\omega t) \right]^{1/2}$$

$$= \left[ \frac{V_m}{4\pi} \int_0^{2\pi} [1 - \cos 2\omega t] \cdot d(\omega t) \right]^{1/2}$$

$\therefore V_0 = 0$  at  $0 \leq \omega t \leq \alpha$  &  $\pi \leq \omega t < 2\pi$

$$\therefore (V_0)_{\text{rms}} = \left[ \frac{V_m}{4\pi} \int_{\alpha}^{\pi} (1 - \cos 2\omega t) \cdot d(\omega t) \right]^{1/2}$$

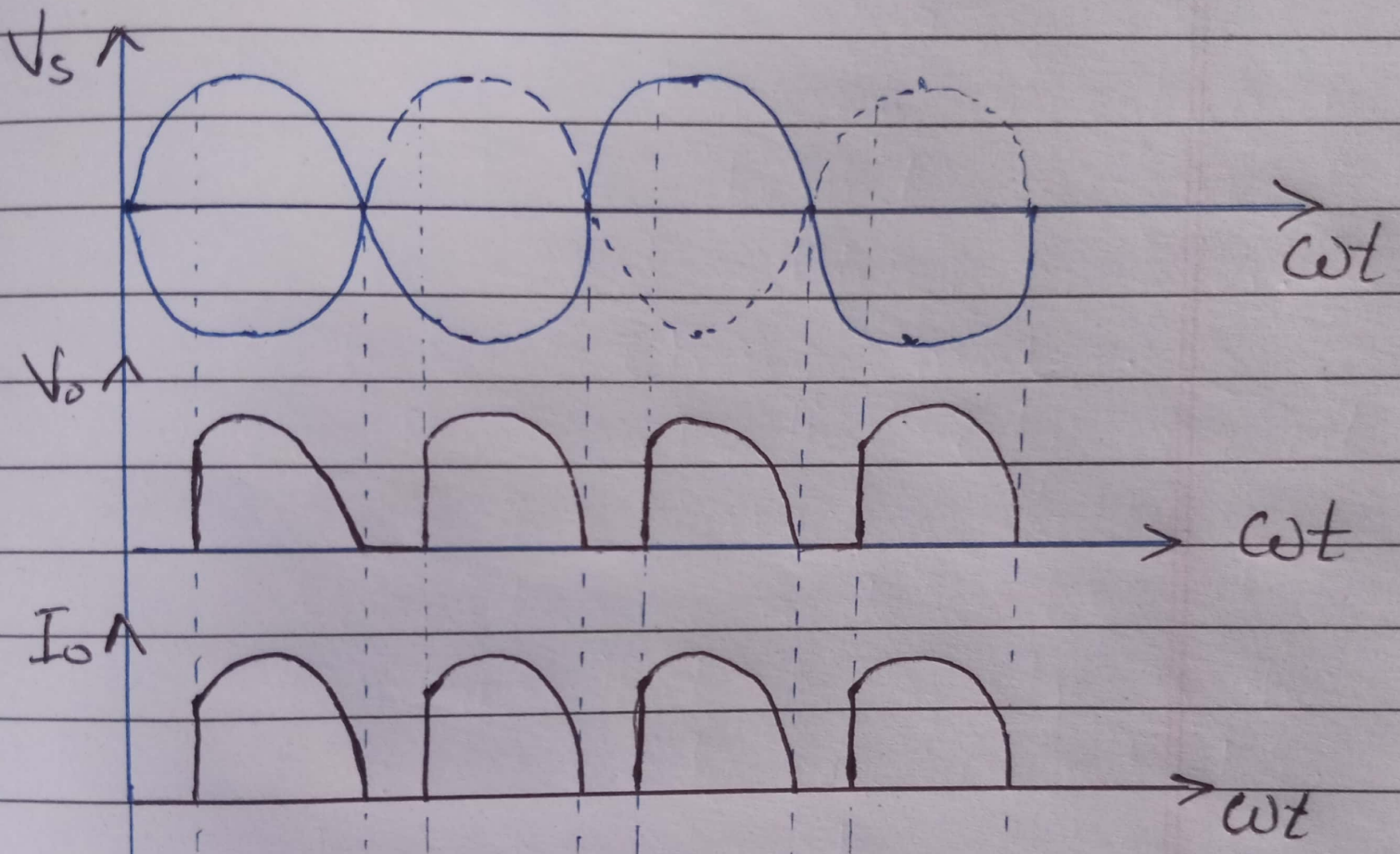
$$= \frac{V_m}{2\sqrt{\pi}} \sqrt{(\pi - \alpha) + \frac{1}{2} \sin 2\alpha}$$

$$V_{\text{or}} = \frac{V_m}{2\sqrt{\pi}} \left[ (\pi - \alpha) + \frac{1}{2} \sin 2\alpha \right]^{1/2}$$

$$I_{\text{or}} = \frac{V_{\text{or}}}{R}$$

Power delivered to resistive load

$$= V_{\text{or}} \cdot I_{\text{or}} = \frac{V_{\text{or}}^2}{R}$$



Waveform of  $1\phi$  full wave rectifier.